3D GRAPHIC STATICS VIA GRASSMANN ALGEBRA

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METHODS OF GRAPHIC STATICS ARE USED FOR SOLVING PROBLEMS OF STATICS, EVALUATION OF EQUILIBRIUM AND DETERMINATION OF INTERNAL FORCES AS WELL AS FORCES IN SUPPORTS OF STRUCTURAL SYSTEMS BY APPLYING ONLY GEOMETRICAL OPERATIONS. THEY ARE BASED ON CONSTRUCTION OF TWO RECIPROCAL DIAGRAMS, THE FORM DIAGRAM WHICH SHOWS THE GEOMETRY OF STRUCTURE (LOCATION OF INTERNAL NODES AND SUPPORTS, EXTERNAL LOADS AND LENGTHS OF STRUCTURAL ELEMENTS) AND THE FORCE DIAGRAM WHERE POLYGONS OF FORCES, ASSEMBLED OF VECTORS, REPRESENT EQUILIBRIUM OF INTERNAL FORCES IN STRUCTURAL ELEMENTS, FORCES IN SUPPORTS AND EXTERNAL LOADS. RELATION OF THE TWO RECIPROCAL DIAGRAMS ALLOWS SIMULTANEOUS CONTROL OVER THE SHAPE OF THE STRUCTURE AND INTERNAL FORCES IN STRUCTURAL ELEMENTS AND THUS FINDING AN EFFICIENT GEOMETRY OF THE STRUCTURE AT AN EARLY STAGE OF STRUCTURAL DESIGN PROCESS.

DEVELOPED IN 19TH CENTURY, METHODS OF GRAPHIC STATICS WERE LIMITED ONLY TO PLANAR AND SIMPLE SPATIAL PROBLEMS OF STATICS. OWING TO TODAY'S ADVANCED TOOLS FOR COMPUTER-AIDED DESIGN (CAD), THE DEVELOPMENT AND APPLICATION OF THE METHODS OF THREE-DIMENSIONAL (3D) GRAPHIC STATICS, SUCH AS 3D ALGEBRAIC POLYHEDRAL GRAPHIC STATICS AND 3D VECTOR-BASED GRAPHIC STATICS, BOTH BASED ON IDEAS FROM 19TH CENTURY, ARE AVAILABLE.





HERMANN GRASSMANN'S GREAT CONTRIBUTION TO MATHEMATICS AND MECHANICS WAS HIS CONCEPT OF COORDINATIZATION OF HIGHER DIMENSIONAL SUBSETS (SUBSPACES) OF GEOMETRICAL SETS, AND JULIUS PLÜCKER IS RESPONSIBLE FOR APPLICATION OF THESE IDEAS TO THE SET OF LINES IN THE EXTENDED EUCLIDEAN SPACE.

HERMANN GRASSMANN (1809. - 1877.) AND JULIUS PLÜCKER (1801. - 1868.

EXTENDED EUCLIDEAN SPACE

WITH THIS ONE LINE, WHICH IS THEN ITS INTERSECTION WITH ALL OTHER PLANES PARALLEL TO IT, AND EVERY LINE IN SPACE CONTAINS, OR IS EXTENDED BY, ONE IDEAL POINT SO THAT THIS POINT IS ITS INTERSECTION WITH ALL OTHER LINES PARALLEL TO IT. THIS KIND OF SPACE IS CALLED THE EXTENDED EUCLIDEAN SPACE $P^3(\mathbb{R})$, and it is a 3-dimensional projective space. The points of the extended Euclidean space are either the points of the Euclidean space E^3 OR THE IDEAL POINTS, AND THE ENTIRE E^3 IS CANONICALLY EMBEDDED IN $P^3(\mathbb{R})$ AS THE COMPLEMENT OF THE IDEAL PLANE. IT IS ALSO EMBEDDED IN THE VECTOR SPACE \mathbb{R}^4 OR EQUIVALENTLY, WE CAN THINK OF IT AS AN IMAGE OF PROJECTION OF \mathbb{R}^4 INTO THREE DIMENSIONS WHICH CAN BE DONE IN INFINITELY MANY WAYS.

In the usual Cartesian coordinate system of \mathbb{R}^4 , with four mutually orthogonal axes, a vector $\mathbf{x} = (x_0, x_1, x_2, x_3)$ is given by its coordinates x_0 , x_1 , x_2 , x_3 WHICH REPRESENT PROJECTIONS OF THIS VECTOR TO THE FOUR AXES. WE DENOTE THE ONE-DIMENSIONAL SUBSPACE, THE SPAN OF THIS VECTOR, BY $\langle x \rangle$ AND IT IS A LINE OF \mathbb{R}^4 PASSING THROUGH THE ORIGIN POINT.

Then the **homogenous coordinates** of the corresponding point in $P^3(\mathbb{R})$ are denoted by $(x_0:x_1:x_2:x_3)$ and the homogeneity property states

 $\lambda(x_0: x_1: x_2: x_3) = (\lambda x_0: \lambda x_1: \lambda x_2: \lambda x_3) = (x_0: x_1: x_2: x_3), \quad \lambda \neq 0, \quad \lambda \in \mathbb{R}$

MUST BE TRUE FOR EVERY VECTOR IN \mathbb{R}^4

HAVING IN MIND THE FIRST PARAGRAPH, WE USUALLY CHOOSE THE FIRST VARIABLE x_0 , THUS THE SET OF IDEAL POINTS BECOMES THE PLANE OF $P^3(\mathbb{R})$ HAVING THE EQUATION $x_0 = 0$, and the Euclidean space E^3 is isomorphic to its complement, a set given with the equation $x_0 \neq 0$, and is the image of the **PROJECTION**

 $(x_0: x_1: x_2: x_3) = \left(1: \frac{x_1}{x_0}: \frac{x_2}{x_0}: \frac{x_3}{x_0}\right) = \left(\frac{x_1}{x_0}, \frac{x_2}{x_0}, \frac{x_3}{x_0}\right)$

FROM THAT SET.

The homogenous coordinates of a plane $(\alpha_0:\alpha_1:\alpha_2:\alpha_3)$ are interpreted in E^3 as the plane passing through the points $(\alpha_1,0,0)$, $(0,\alpha_2,0)$ and $(0,0,\alpha_3)$, its intersections with the coordinate axes, unless the first coordinate $\alpha_0=0$ in which case the plane contains the origin point. The IDEAL PLANE IS GIVEN BY $(\alpha_0:0:0:0)$ WITH $\alpha_0 \neq 0$.

INCIDENCE RELATION

IN THE PROJECTIVE SPACE, ON THE SET OF BASIC ELEMENTS - POINTS, LINES AND PLANES WE HAVE THE INCIDENCE RELATION. THIS SPACE CAN BE AXIOMATICALLY DESCRIBED WITH AXIOMS OF INCIDENCE IF WE WANT TO EMPLOY SYNTHETIC GEOMETRY, OR WE CAN EXPLORE IT ANALYTICALLY, WHICH WE WILL, USING HOMOGENOUS COORDINATES

THE INCIDENCE RELATION HAS THREEFOLD INTERPRETATIONS, THREE ASPECTS. FIRST IS RELATION ITSELF IN A PASSIVE SENSE, TO BE INCIDENT MEANING TO LIE IN OR TO PASS THROUGH, NOTING THE RELATION BETWEEN ELEMENTS OF THE SPACE. THE OTHER TWO ARE ACTIVE, USED TO DEFINE AN ELEMENT WITH OTHER LOWER OR HIGHER DIMENSIONAL ELEMENTS. FIRST IS THE MEET OR INTERSECTION, FOR INSTANCE TWO LINES MEET OR INTERSECT AT A POINT, AND THE OTHER IS THE JOIN OR SPAN, FOR INSTANCE THE SPAN OF TWO POINTS IS A LINE, OR THE LINE IS GIVEN AS A JOIN OF TWO POINTS.

GRASSMANN'S OUTER PRODUCT

GRASSMANN DEFINED AN OPERATION, WHICH HE NAMED OUTER PRODUCT, THAT TAKES TWO ELEMENTS OF THE VECTOR SPACE AND ATTACHES TO THIS PAIR ONE ELEMENT OF ANOTHER, HIGHER DIMENSIONAL, VECTOR SPACE. THE ADJECTIVE "OUTER" THUS EXPRESSING THAT THE RESULT OF THE OPERATION IN NOT CONTAINED IN THE SAME VECTOR SPACE AS THE OPERANDS.

HE THEN PRESCRIBES TWO PROPERTIES THAT THIS OPERATION MUST SATISFY SO THAT THE RESULTING VECTOR SPACE IS UNIQUELY DETERMINED - THIS

OPERATION IS ANTI-COMMUTATIVE AND LINEAR IN BOTH ARGUMENTS, BILINEAR. WE PRESENT HIS CONSTRUCTION FOR \mathbb{R}^4 and k=2. Let e_i be the elements of canonical basis for \mathbb{R}^4 . We denote the outer product of two

ELEMENTS e_i AND e_i BY e_i A e_i AND FOR ALL ELEMENTS $\mathbf{x} = x_0 e_0 + x_1 e_1 + x_2 e_2 + x_3 e_3$ AND $\mathbf{y} = y_0 e_0 + y_1 e_1 + y_2 e_2 + y_3 e_3$ IN \mathbb{R}^4 WE HAVE

$$x \wedge y = (x_0 y_1 - x_1 y_0) e_0 \wedge e_1 + (x_0 y_2 - x_2 y_0) e_0 \wedge e_2 + (x_0 y_3 - x_3 y_0) e_0 \wedge e_3 + (x_2 y_3 - x_3 y_2) e_2 \wedge e_3 + (x_3 y_1 - x_1 y_3) e_3 \wedge e_1 + (x_1 y_2 - x_2 y_1) e_1 \wedge e_2$$

WE RELATE THE INCIDENCE RELATION TO THE CONCEPT OF THE OUTER PRODUCT, THE BILINEAR OPERATION OF GRASSMANN ALGEBRA. FIRST, THE MEET OPERATION, WHICH DEFINES ELEMENTS OF $P^3(\mathbb{R})$ USING LOWER DIMENSIONAL ELEMENTS IS CORRESPONDENT, IN GRASSMANN'S TERMINOLOGY, TO THE PROGRESSIVE PRODUCT. FOR INSTANCE, A LINE, IN GRASSMANN GEOMETRICAL ALGEBRA, CAN BE DEFINED AS OUTER PRODUCT OF TWO POINTS. THE ADJECTIVE PROGRESSIVE EMPHASIZING THAT THIS DEFINITION STARTS WITH LOWER AND RESULTS IN HIGHER DIMENSIONAL ELEMENTS, OR SUBSPACES ANALOGOUSLY, GIVEN THE DUALITY PRINCIPLE. A LINE GEOMETRICALLY DEFINED AS INTERSECTING LINE OF TWO PLANES CAN BE DEFINED AS OUTER PRODUCT OF TWO PLANES. THIS KIND OF OUTER PRODUCT, WHERE WE START WITH HIGHER AND END UP WITH LOWER DIMENSIONAL OBJECTS IS, IN GRASSMANN'S TERMINOLOGY, NOTED AS REGRESSIVE PRODUCT.

TABLE COMPUTING WITH HOMOGENOUS COORDINATES

 $x \in \alpha \iff$

 $x_0 \alpha_0 + \bar{x}\bar{\alpha} = 0$

 $L = \langle x, y \rangle \iff$

 $L = (x_0 \bar{y} - y_0 \bar{x}, x \times y)$

 $\alpha = \langle L_1, L_2 \rangle \iff$

 $\boldsymbol{\alpha} = (\ \boldsymbol{l}_1 \cdot \boldsymbol{l}_2, -\boldsymbol{l}_1 \times \boldsymbol{l}_2)$

 $x = \alpha \cap L \Leftrightarrow$

 $x = (\alpha \cdot l, -\alpha_0 l + x \times \overline{l})$

 $x \in L \iff$

 $x \cdot l = 0$ and

 $-x_0\bar{\boldsymbol{l}} + \boldsymbol{x} \times \boldsymbol{l} = 0$

 $L = \alpha \cap \beta \iff$

 $L = (\boldsymbol{\alpha} \times \boldsymbol{\beta}, \alpha_0 \bar{\beta} - \beta_0 \bar{\alpha})$

 $x = L_1 \cap L_2 \iff$

 $\mathbf{x} = (\mathbf{l}_1 \cdot \overline{\mathbf{l}_2}, -\overline{\mathbf{l}_1} \times \overline{\mathbf{l}_2})$

 $\alpha = \langle x, L \rangle \iff$

 $\alpha = (x \cdot \bar{l}, -x_0\bar{l} + x \times l)$

A LINE L INTERPRETED AS THE PROGRESSIVE PRODUCT OF TWO POINTS $L = x \land y$ has Grassmann coordinates $L = (l_{01}, l_{02}, l_{03}, l_{23}, l_{31}, l_{12}) \in \Lambda^2 \mathbb{R}^4$ where

FOR $(i,j) \in \{(0,1),(0,2),(0,3),(2,3),(3,1),(1,2)\}$ and the following relation, **Plücker relation** must hold: $l_{01}l_{23} + l_{02}l_{31} + l_{03}l_{12} = 0$.

THE PLÜCKER COORDINATES OF A LINE ARE THE HOMOGENOUS COORDINATES $(l_{01}: l_{02}: l_{03}: l_{23}: l_{12}) = (\boldsymbol{l}, \boldsymbol{l}),$ WHERE $m{l}=(l_{01},l_{02},l_{03})$ and $m{ar l}=(l_{23},l_{31},l_{12})$ and the Plücker relation now reads $m{l}\cdotm{ar l}=0$.

IN THE TABLE ON THE RIGHT WE PRESENT THE FORMULAS IN HOMOGENOUS COORDINATES FOR THE FOLLOWING INCIDENCE **RELATIONS:**

- A POINT INCIDENT WITH (LYING IN) A PLANE, A POINT INCIDENT WITH (LYING ON) A LINE,
- A LINE AS JOIN OF TWO POINTS,
- A LINE AS MEET OF TWO PLANES, A POINT AS MEET OF TWO INTERSECTING LINES,
- A PLANE AS JOIN OF TWO INTERSECTING LINES,
- A PLANE AS JOIN OF A POINT AND NON-INCIDENT LINE AND A POINT AS MEET OF A LINE AND NON-INCIDENT PLANE

THESE FORMULAS CAN BE EASILY VERIFIED BY DIRECT COMPUTATION USING VECTOR CALCULUS. WE WRITE THE HOMOGENOUS COORDINATES OF POINTS AND PLANES AS

 $x = (x_0 : x_1 : x_2 : x_3) = (x_0, \bar{x})$

 $\boldsymbol{\alpha} = (\alpha_0 : \alpha_1 : \alpha_2 : \alpha_3) = (\alpha_0, \bar{\alpha}),$

THUS, EMPHASIZING STANDARD CARTESIAN COORDINATES OF POINTS IN E³, I.E. NORMAL VECTORS OF PLANES.

HOMOGENOUS COORDINATES OF LINES ARE AS IN (1).

FORCE COORDINATES

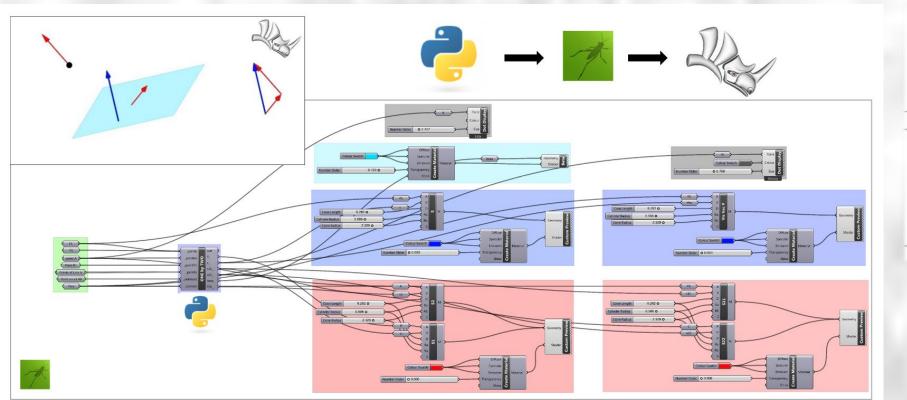
SINCE A FORCE ACTING AT A POINT IN THE SPACE IS LYING ON A LINE AND DUE TO THE PRINCIPLE OF TRANSMISSIBILITY, WE CAN USE THE LINE PLÜCKER COORDINATES TO DERIVE THE COORDINATES FOR A FORCE. THIS IS DONE BY THE FURTHER REMARK ON THE GEOMETRICAL INTERPRETATION OF THE COORDINATES; THE VECTOR $ar{l}$ IS ORTHOGONAL TO THE VECTOR $ar{l}$ AND CAN BE INTERPRETED AS THE MOMENT VECTOR ABOUT THE ORIGIN POINT OF THE COORDINATE SYSTEM OF A FORCE F LYING ON THE LINE. FURTHERMORE, THE IDEAL POINT OF THIS LINE IS THE POINT $(0:l_{01}:l_{02}:l_{03})$, IN OTHER WORDS THE VECTOR \boldsymbol{l} REPRESENTS THE DIRECTION OF THE LINE, AND IF

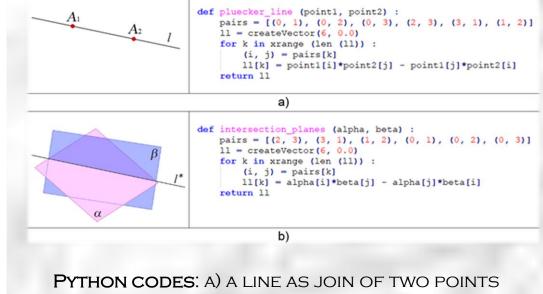
POINT IN E^3 . Therefore, a force F can be given by its coordinates $F = (f, \overline{f})$, with f being is force vector and \overline{f} its moment vector about the origin point OF THE COORDINATE SYSTEM. THESE COORDINATES ARE NOT HOMOGENOUS SINCE THE QUANTITY ||f|| REPRESENTS ITS INTENSITY.

 $x = (1: x_1: x_2: x_3)$ is any other (non-ideal) point on the line, then we have $\bar{l} = x \times l$, with $x = (x_1, x_2, x_3)$ being the Cartesian coordinates of the

FOR PERFORMANCE AND VISUALISATION OF THE EXAMPLES OF STATIC EQUIVALENCE AND THE EXAMPLES OF EQUILIBRIUM FINDING THAT WE PRESENT, WE HAVE DEVELOPED A COMPUTER PROGRAM BASED ON ALGEBRAIC TRANSLATIONS OF INCIDENCE OPERATIONS USING CAD TOOL RHINOCEROS. STEPS OF THE GRAPHICAL PROCEDURES ARE CARRIED OUT USING BASIC OPERATIONS OF INCIDENCE GEOMETRY, WHICH CAN BE EASILY EXPRESSED IN ALGEBRAIC FORM USING GRASSMANN ALGEBRA, THUS ENABLING THEIR CONVERSION INTO A PROGRAMME CODE.

THE PROGRAMME CODE IS WRITTEN IN GHPYTHON (PYTHON INTERPRETER AND PLUG-IN FOR GRASSHOPPER), AND THE RESULTS ARE VISUALIZED IN RHINOCEROS (PROCESS IS DESCRIBED IN THE FIGURE BELLOW). ALL PROCEDURES OF STATIC EQUIVALENCE AND GEOMETRICAL CONSTRUCTIONS ARE GRAPHICALLY PERFORMED IN FORM DIAGRAM AND THEN FOLLOWED BY FORCE POLYGONS IN THE FORCE DIAGRAM.



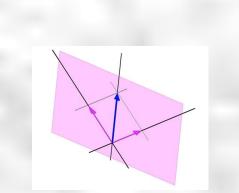


B) A LINE AS MEET OF TWO PLANES

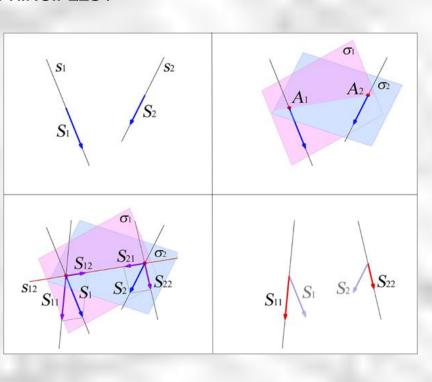
EXAMPLES

GIVEN FORCE SYSTEM DESCRIBED HERE ARE CARRIED OUT USING GEOMETRIC CONSTRUCTIONS WHICH CAN BE CONSIDERED AS A PARTIAL THREE-DIMENSIONAL EXTENSION OF FUNICULAR POLYGON CONSTRUCTION. THE EXTENSION OF FUNICULAR POLYGON IS BASED ON TWO PRINCIPLES

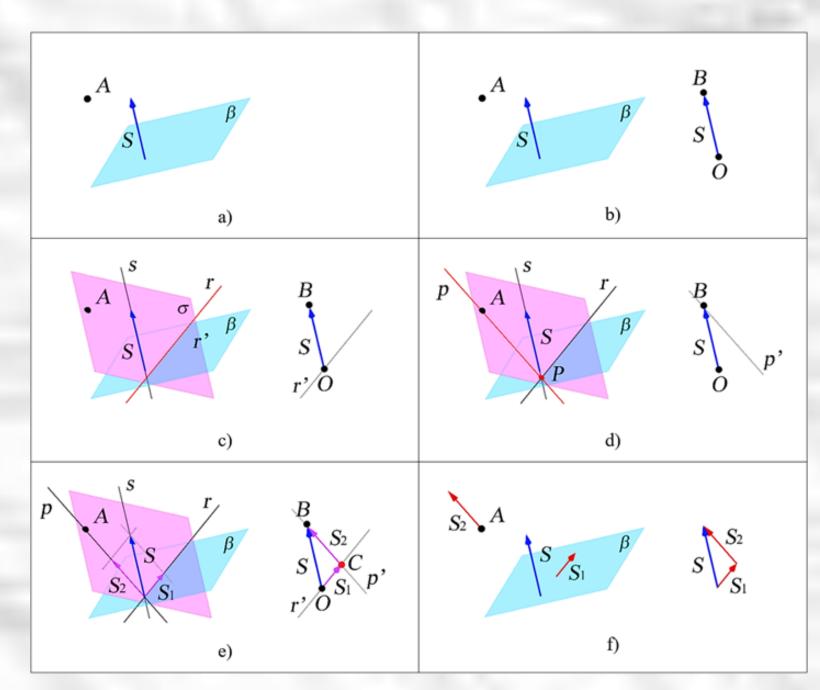
1) SINGLE FORCE CAN BE RESOLVED INTO TWO FORCE COMPONENTS ALONG TWO GIVEN LINES IF AND ONLY IF ITS LINE OF ACTION AND TWO GIVEN LINES ARE CONCURRENT AND COPLANAR



2) GENERALLY. CONDITION, EACH OF TWO GIVEN FORCES IS RESOLVED INTO TWO COMPONENTS IN SUCH A



• REPLACING SINGLE FORCE WITH A FORCE ACTING AT A GIVEN POINT AND A FORCE LYING IN A GIVEN PLANE



IN THIS EXAMPLE, WE WILL ALSO SHOW TRANSLATIONS OF GEOMETRIC OPERATIONS INTO GRASSMANN ALGEBRA EXPRESSIONS.

A PLANE σ IS A JOIN OF THE GIVEN POINT A AND THE LINE OF ACTION S OF THE GIVEN FORCE S (IN ALGEBRAIC TERMS: JOIN $\sigma = [A \land S]$) FIRST COMPONENT OF THE FORCE S ACTS ALONG THE LINE R, WHICH

(MEET R = $[\sigma \land \beta]$) SECOND COMPONENT ACTS ALONG THE CONNECTING LINE P OF THE POINT A AND THE INTERSECTION POINT P OF THE LINE S AND THE PLANE β (MEET AND THEN JOIN: $P = [S \land \beta], P = [A \land P]$) (Figure

IS THE INTERSECTION LINE OF THE PLANE σ AND A GIVEN PLANE β

PREVIOUS STEPS WERE PERFORMED IN THE FORM DIAGRAM WHILE THE FOLLOWING ONES WILL BE PERFORMED IN THE FORCE DIAGRAM. FROM ARBITRARILY CHOSEN POINT O VECTOR S OF THE FORCE S IS DRAWN; HEAD OF S IS THE POINT B (B = O + s).

LINES R' AND P' ARE DRAWN THROUGH O AND B PARALLEL TO THE LINES R AND P (R' = $[O \land R]$, P' = $[B \land P]$, WHERE R AND P ARE SOME VECTORS ON LINES R AND P). LINES R' AND P' INTERSECT IN THE POINT C ($C = [R' \land P']$) (FIGURE E).

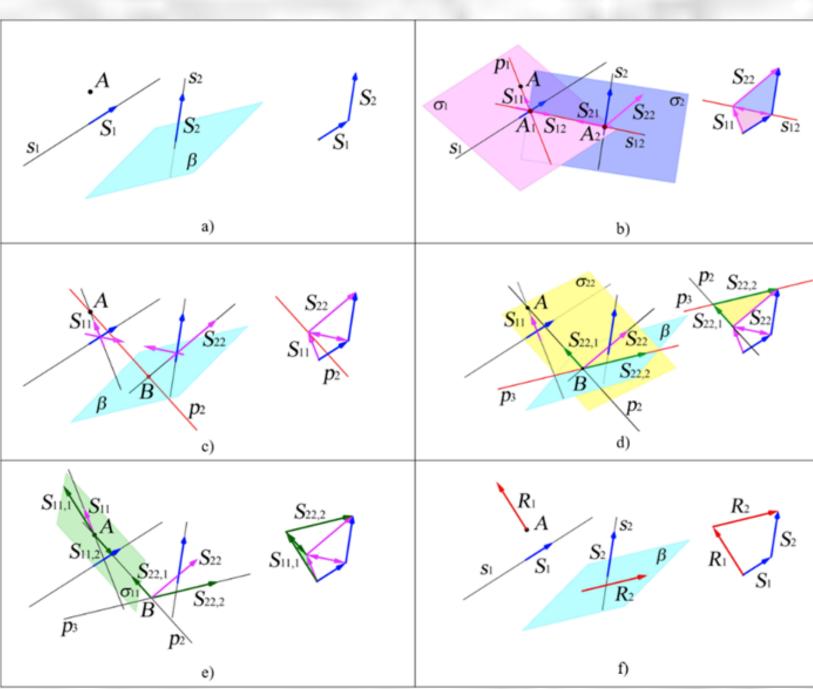
VECTORS S1 AND S2 OF FORCE COMPONENTS S1 AND S2 ON LINES R AND P ARE $S_1 = C - O$ AND $S_2 = B - C$.

REPLACING TWO FORCES WITH A FORCE ACTING AT A GIVEN POINT AND A FORCE LYING IN A GIVEN PLANE

THEOREM THAT "ANY SYSTEM OF FORCES CAN ALWAYS BE REPRESENTED BY TWO FORCES ONE OF WHICH LIES IN A GIVEN PLANE, AND THE OTHER PASSES THROUGH A GIVEN POINT NOT LYING IN THE PLANE" WAS ALSO PROVED BY WHITEHEAD [5].

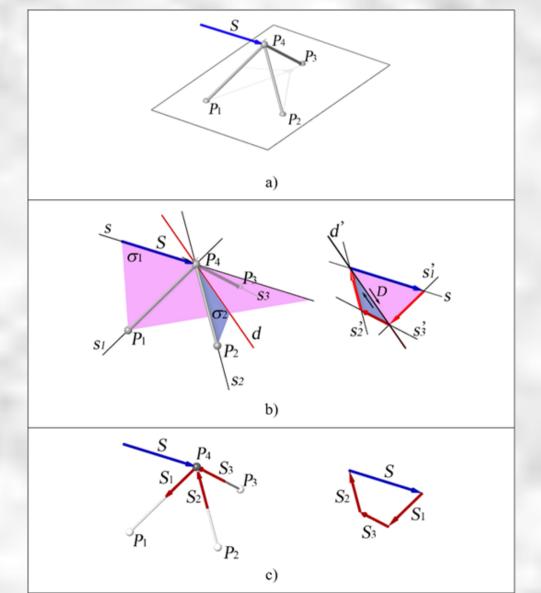
THE FIRST PROCEDURE FOR REPLACING TWO FORCES WITH A FORCE ACTING AT A GIVEN POINT AND A FORCE LYING IN A GIVEN PLANE IS TO RESOLVE EACH OF TWO GIVEN FORCES S1 AND S2 INTO A COMPONENT ACTING AT THE GIVEN POINT A AND A COMPONENT LYING IN A GIVEN PLANE β. THE RESULTANT R₁ OF THE TWO COMPONENTS ACTS AT THE POINT A AND THE RESULTANT R2 OF THE OTHER TWO COMPONENTS LIES IN THE PLANE β. TWO OBTAINED FORCES ARE STATICALLY EQUIVALENT TO THE GIVEN FORCES S_1 AND S_2 .

ANOTHER PROCEDURE, SIMILAR TO THE FUNICULAR POLYGON CONSTRUCTION, IS AS FOLLOWS. S1 AND S2 ARE GIVEN FORCES ACTING ON LINES S₁ AND S₂ (FIGURE A). THE PLANE σ_1 IS DEFINED BY THE GIVEN POINT A AND THE LINE S1, AND THE PLANE σ_2 BY THE LINE S2 AND A POINT A1 ARBITRARILY CHOSEN ON THE LINE S1. THE LINE S12 IS THE INTERSECTION OF THE PLANES σ_1 AND σ_2 . (THE LINE S_{12} CAN ALSO BE CONSIDERED AS A CONNECTING LINE BETWEEN TWO ARBITRARILY CHOSEN POINTS, A₁ ON THE LINE S₁ AND A₂ ON THE LINE S₂.) THE COMPONENT S₁₂ OF THE FORCE S₁ AND THE COMPONENT S₂₁ OF THE FORCE S2 ACT ALONG THE SAME LINE S12 AND CANCEL EACH OTHER. SECOND COMPONENT S11 OF THE FORCE S1 ACTS ALONG THE LINE P1 CONNECTING THE POINTS A AND A1. NOW, THE FORCE S_2 can be resolved in the plane σ_2 . In that way given FORCES S_1 AND S_2 ARE REPLACED WITH THE FORCES S_{11} AND S₂₂ (FIGURE B).



THE POINT B IS THE INTERSECTION OF THE LINE OF ACTION OF THE FORCE S_{22} , LINE S_{22} , AND THE GIVEN PLANE β . Span (or join) of two points A and B is THE LINE P2 (FIGURE C). THE PLANE σ_{22} IS DEFINED AS A JOIN OF THE LINES S22 AND P2. PLANES σ_{22} AND β INTERSECT IN THE LINE P3. Now, we resolve the force S22 into two components S22,1 and S22,2 along the lines P2 and P3 (Figure D), and the force S11 into components S11,1 AND $S_{11,2} = -S_{22,1}$ (FIGURE E). REMAINED COMPONENTS $S_{11,1} = R_1$, A FORCE WHICH ACTS AT THE GIVEN POINT A, AND $S_{22,2} = R_2$, A FORCE WHICH LIES IN THE GIVEN PLANE β (FIGURE F), REPRESENT EQUIVALENT FORCE SYSTEM TO THE SYSTEM OF FORCES S1 AND S2. REVERSION OF THE OBTAINED FORCES R1 AND R2 GIVES EQUILIBRATING FORCES TO THE GIVEN TWO-FORCE SYSTEM.

EQUILIBRIUM OF A SPATIAL NODE



HERE, WE DESCRIBE AN EXAMPLE OF FINDING EQUILIBRIUM OF A GIVEN SPATIAL NODE P4 SUPPORTED BY THREE BARS P₁P₄ (LINE S₁), P₂P₄ (LINE S₂) AND P₃P₄ (LINE S₃). THE BARS ARE CONNECTED TO THE GROUND WITH SPHERICAL SUPPORTS P1, P2 AND P3. ALSO, THE NODE P4 IS A SPHERICAL NODE AT WHICH GIVEN FORCE S ACTS ALONG ITS LINE OF ACTION S (FIGURE A).

THE PROCEDURE FOR EQUILIBRIUM FINDING OF A SPATIAL NODE IS SIMILAR TO THE PROCEDURE FOR REPLACING A SINGLE FORCE WITH THREE FORCES ACTING ALONG BARS P1P4, P2P4 AND P3P4. IN THE FORM DIAGRAM (FIGURE B), WE DEFINE PLANE σ1 CONTAINING THE LINE OF ACTION S AND THE LINE S2, AND PLANE σ_2 CONTAINING THE LINES S1 AND S3. THE INTERSECTION LINE OF THE PLANES σ_1 AND σ_2 IS THE LINE D. NOW, ALL THE LINES IN THE FORM DIAGRAM ARE KNOWN, THUS THE PROCEDURE IS CARRIED OUT IN THE FORCE DIAGRAM (FIGURE B, ON THE RIGHT SIDE).

FIRST, WE PLACE THE LINE S2' PARALLEL TO THE LINE S2 AT THE TAIL OF THE FORCE S, AND AT THE HEAD OF THE FORCE S, WE PLACE THE LINE D' PARALLEL TO THE LINE D. SINCE THE FORCE $D = S+S_1$ IS THE SUM OF THE FORCES S AND S1, AND SINCE ALL OF THEM LIE IN THE PLANE PARALLEL TO THE PLANE σ_1 , THE INTERSECTION OF TWO LINES GIVES THE POINT WHICH DEFINES MAGNITUDES OF THE FORCES D AND S1. THE COMPONENT S1 ACTS ALONG THE LINE S1, AND THE FORCE D ACTS ALONG THE LINE D'. IN THAT WAY S1 AND D ARE DETERMINED. NOW, RESULTANT FORCE OF THE FORCES S2 AND S3 MUST BE IN EQUILIBRIUM WITH THE FORCE D. IT IS WELL KNOWN THAT TWO FORCES ARE IN EQUILIBRIUM IF THEY ACT ALONG THE SAME LINE, THEY ARE OPPOSITE IN SENSE AND EQUAL IN MAGNITUDE. THUS, THE FORCE D AND THE FORCE -D=S2+S3 ACT ALONG THE LINE D' AND CANCEL EACH OTHER OUT. AGAIN, IN THE FORCE DIAGRAM, WE PLACE A LINE S2' AT THE TAIL OF THE FORCE -D PARALLEL TO THE LINE S2 AND AT THE HEAD OF THE FORCE -D WE PLACE A LINE S3' PARALLEL TO THE LINE S3. SINCE ALL THE FORCES \overline{D} , S2 AND S3 LIE IN THE SAME PLANE PARALLEL TO THE PLANE σ_2 , THE INTERSECTION POINT OF THE LINES S2' AND S3' DETERMINES FORCES S2 AND S3. IN THAT WAY FORCES S, S₁, S₂ AND S₃ FORM A CLOSED POLYGON IN THE FORCE DIAGRAM, I.E. THE SPATIAL NODE P₄ IS IN EQUILIBRIUM (FIGURE C).

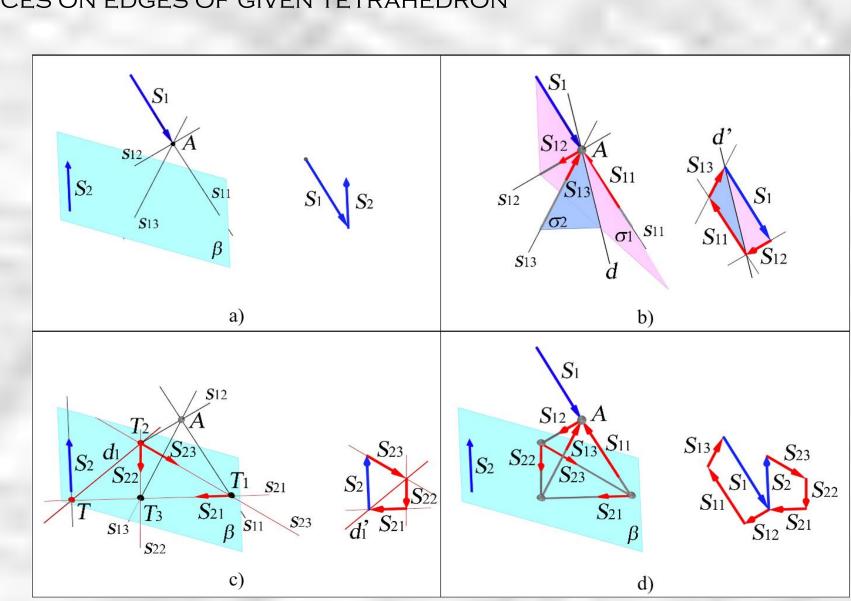
EQUILIBRATING TWO-FORCE SYSTEM WITH FORCES ON EDGES OF GIVEN TETRAHEDRON

FORCES S1 AND S2 ARE TWO GIVEN FORCES. THE FORCE S1 ACTS AT THE GIVEN POINT A AND THE FORCE S2 LIES IN THE GIVEN PLANE β (FIGURE A). THREE LINES S11, S12 AND S13 ARE GIVEN THROUGH THE SAME POINT A, AND LINES S21, S22 AND S23 ARE LYING IN THE PLANE β .

IN OUR CASE, THE SIX LINES ARE GIVEN IN A SPECIAL POSITION, THAT IS THEY ARE EDGES OF A TETRAHEDRON. FOR EACH OF THE GIVEN FORCES, THREE EQUILIBRATING FORCES WILL BE

FOR THE FORCE S₁, USING THE PROCEDURE FOR FINDING EQUILIBRIUM OF A SPATIAL NODE DESCRIBED IN THE PREVIOUS SUBSECTION, THREE EQUILIBRATING FORCES S11, S12 AND S13, ACTING ALONG THE GIVEN LINES S11, S12 AND S13 AT THE SAME POINT A, WHICH IS ALSO A VERTEX OF THE TETRAHEDRON, WILL BE DETERMINED (FIGURE B).

For the force S_2 three forces act in the same plane β ALONG THE GIVEN LINES S21, S22 AND S23. IN THIS SPECIAL POSITION, POINTS T₁, T₂ AND T₃ ARE VERTICES OF THE GIVEN TETRAHEDRON AND ALSO INTERSECTION POINTS OF THE LINES S_{11} , S_{12} AND S_{13} WITH THE PLANE β IN GENERAL CASE. SINCE ALL LINES, ALONG WHICH THE THREE EQUILIBRATING FORCES S21, S₂₂ AND S₂₃ TO THE FORCE S₂ ACT, ARE KNOWN, THEY CAN BE DETERMINED IN THE FORCE DIAGRAM. THE LINE D1, CONNECTING THE INTERSECTION POINT T2 OF THE LINES OF ACTION OF THE FORCES S22 AND S23 AND THE INTERSECTION POINT T OF THE LINES OF ACTION OF THE FORCES S2 AND S21, REPRESENTS CULMANN'S LINE (FIGURE C). USING WELL-KNOWN METHODS OF PLANAR (2D) GRAPHIC STATICS, WE OBTAIN EQUILIBRATING FORCES S₂₁, S₂₂ AND S₂₃.



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