

GS 2. — 6. veljače 2024.

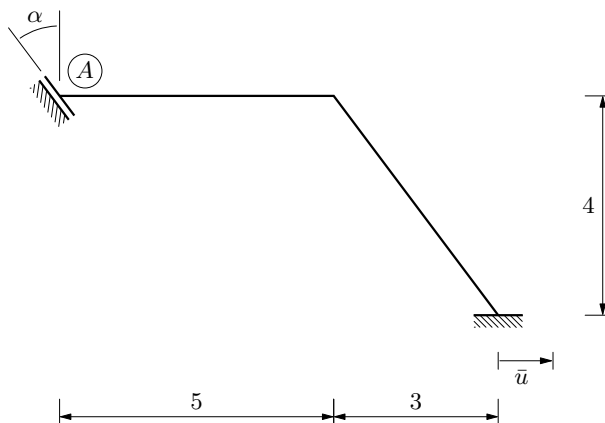
Zadatak 1.

Inženjerskom metodom pomakā nacrtajte dijagrame unutarnjih sila! Izračunajte duljinu pomaka točke A!

$$\operatorname{tg} \alpha = 3/4$$

$$EI = 162000 \text{ kNm}^2$$

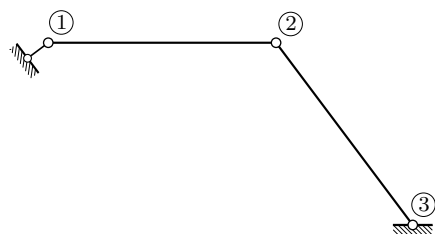
$$\bar{u} = 2 \text{ mm}$$



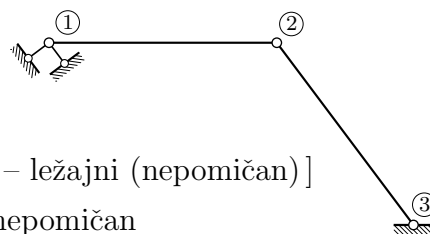
Lipe pred crkvom istom sam nagađao u ogromnim konturama crnih neodređenih masa što su se u tamnoj tamnini još tamnije od ostaloga valovlja tmine za sebe kočile i talasale.

K. S. Gjalski: *Notturmo*

zglobna shema i kinematička analiza zglobne sheme (dodavanje spoj(ev)a s podlogom):



$$s_{\min} = 2 \cdot 2 - 3 = 1$$

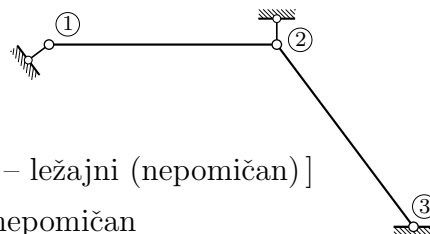


[čvor 3 – ležajni (nepomičan)]

čvor 1 nepomičan

→ čvor 2 nepomičan

ili



[čvor 3 – ležajni (nepomičan)]

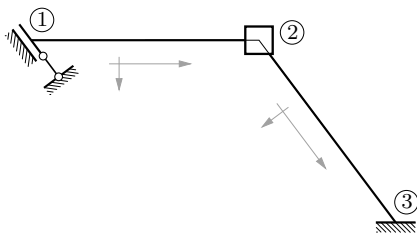
čvor 2 nepomičan

→ čvor 1 nepomičan

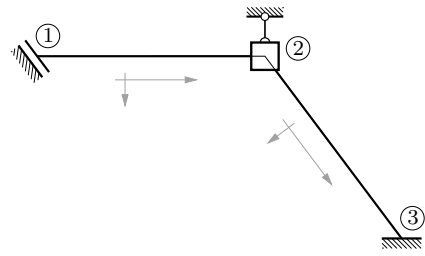
(spoj s podlogom u čvoru 2 može biti na bilo kojem pravcu osim osi štapa {2, 3})

$$\Rightarrow s = s_{\min} = 1$$

osnovni sistem za inženjersku metodu pomakā:



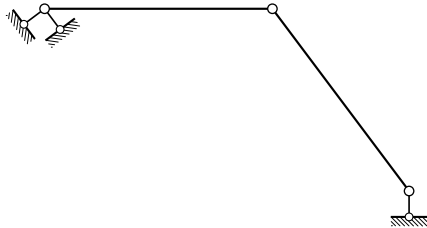
ili



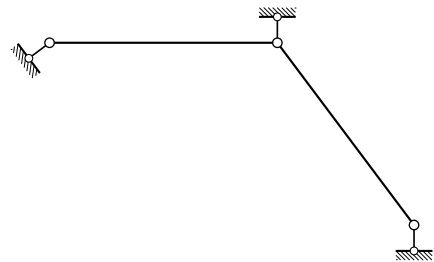
nepoznanice: φ_2 i δ_1 (ili u_1 ili w_1)

nepoznanice: φ_2 i w_2 (ili u_2 ili ...)

mehanizam za utjecaj prisilnoga pomaka ležaja:

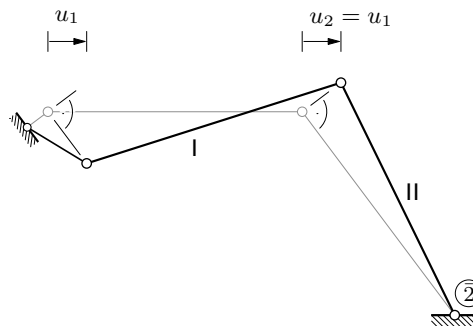


ili

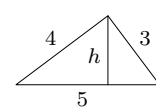
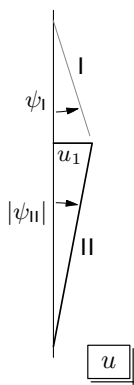
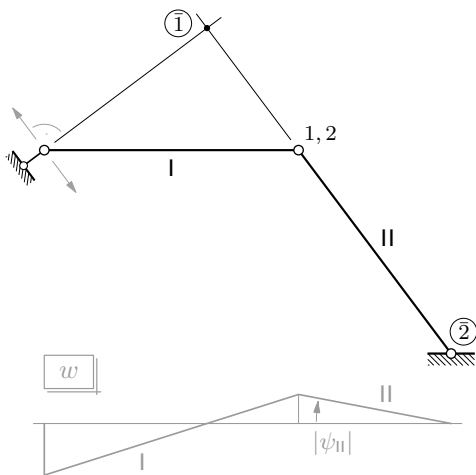


rješavanje pomoću lijevoga osnovnog sistema:

zōra radi, plan pomakā za neovisni translacijski pomak \vec{u}_1 (horizontalnu komponentu pomaka ležaja po kosom pravcu):



izrazi za kutove $\psi_{i,j}$ kao funkcije neovisnoga translacijskog pomaka u_1 (izvedeni pomoću dijagramā projekcijā pomakā na vertikalnu os):



$$\frac{h}{3} = \frac{4}{5}$$

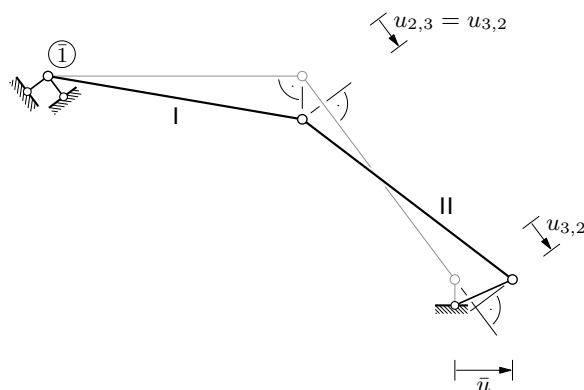
$$h = \frac{12}{5}$$

$$\psi_I = \frac{u_1}{h} = \frac{5}{12} u_1 = \psi_{\{1,2\}}$$

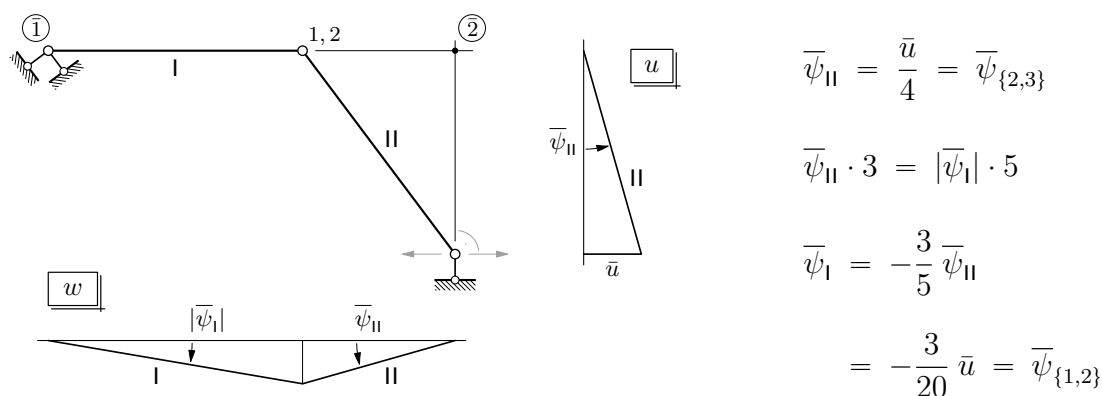
$$\psi_{II} = -\frac{u_1}{4} = \psi_{\{2,3\}}$$

(potpunosti radi, skiciran je i dijagram projekcija pomakā na vertikalnu os)

zōra radi, plan pomakā za prisilni pomak ležaja:



izračunavanje kutova $\bar{\psi}_{i,j}$ pomoću dijagramā projekcijā pomakā na horizontalnu i na vertikalnu os:



vrijednosti momenata upetosti:

$$\begin{aligned} \bar{M}_{1,2} = \bar{M}_{2,1} &= -6 k_{\{1,2\}} \bar{\psi}_{\{1,2\}} = -6 \frac{EI}{5} \left(-\frac{3}{20} \bar{u} \right) \\ &= 6 \cdot \frac{162\,000}{5} \cdot 0,15 \cdot 0,002 = 58,32 \text{ kNm} \end{aligned}$$

$$\bar{M}_{2,3} = \bar{M}_{3,2} = -6 k_{\{2,3\}} \bar{\psi}_{\{2,3\}} = -6 \frac{EI}{5} \frac{\bar{u}}{4} = -6 \cdot \frac{162\,000}{5} \cdot 0,25 \cdot 0,002 = -97,2 \text{ kNm}$$

(izrazi za) vrijednosti momenata savijanja na krajevima štapova:

$$\begin{aligned} M_{1,2} &= 2 k_{\{1,2\}} \varphi_2 - 6 k_{\{1,2\}} \psi_{\{1,2\}} + \bar{M}_{1,2} \\ &= 2 \cdot 32\,400 \varphi_2 - 6 \cdot 32\,400 \cdot \frac{5}{12} u_1 + 58,32 = 64\,800 \varphi_2 - 81\,000 u_1 + 58,32 \end{aligned}$$

$$\begin{aligned} M_{2,1} &= 4 k_{\{1,2\}} \varphi_2 - 6 k_{\{1,2\}} \psi_{\{1,2\}} + \bar{M}_{2,1} \\ &= 4 \cdot 32\,400 \varphi_2 - 6 \cdot 32\,400 \cdot \frac{5}{12} u_1 + 58,32 = 129\,600 \varphi_2 - 81\,000 u_1 + 58,32 \end{aligned}$$

$$\begin{aligned}
M_{2,3} &= 4 k_{\{2,3\}} \varphi_2 - 6 k_{\{2,3\}} \psi_{\{2,3\}} + \overline{M}_{2,3} \\
&= 4 \cdot 32\,400 \varphi_2 - 6 \cdot 32\,400 \left(-\frac{u_1}{4}\right) - 97,2 = 129\,600 \varphi_2 + 48\,600 u_1 - 97,2
\end{aligned}$$

$$\begin{aligned}
M_{3,2} &= 2 k_{\{2,3\}} \varphi_2 - 6 k_{\{2,3\}} \psi_{\{2,3\}} + \overline{M}_{2,3} \\
&= 2 \cdot 32\,400 \varphi_2 - 6 \cdot 32\,400 \left(-\frac{u_1}{4}\right) - 97,2 = 64\,800 \varphi_2 + 48\,600 u_1 - 97,2
\end{aligned}$$

jednadžba ravnoteže momenata u čvoru 2:

$$-M_{2,1} + (-M_{2,3}) = 0 \quad \Big| \quad \times (-1)$$

$$[129\,600 \varphi_2 - 81\,000 u_1 + 58,32] + [129\,600 \varphi_2 + 48\,600 u_1 - 97,2] = 0$$

$$259\,200 \varphi_2 - 32\,400 u_1 - 38,88 = 0$$

jednadžba rada na virtualnim pomacima:

(„vođeći” je virtualni pomak $\delta \vec{u}_1$ koji odgovara neovisnom translacijskom pomaku \vec{u}_1 , pa je dijagram projekcija (virtualnih) pomaka na horizontalnu os jednak dijagramu prikazanom na najdonjoj slici na stranici 2, uz zamjene $u_1 \rightarrow \delta u_1$ i $\psi_i \rightarrow \delta \psi_i$, a veza je kutova $\delta \psi_{\{i,j\}}$ i orijentirane duljine δu_1 ista kao veza $\psi_{\{i,j\}}$ i u_1 :

$$\delta \psi_{\{1,2\}} = 5 \delta u_1 / 12 \quad \mathcal{E} \quad \delta \psi_{\{2,3\}} = -\delta u_1 / 4$$

$$(M_{1,2} + M_{2,1}) \delta \psi_{\{1,2\}} + (M_{2,3} + M_{3,2}) \delta \psi_{\{2,3\}} = 0$$

$$\begin{aligned}
&(64\,800 \varphi_2 - 81\,000 u_1 + 58,32 + 129\,600 \varphi_2 - 81\,000 u_1 + 58,32) \cdot \left(\frac{5}{12} \delta u_1\right) \\
&+ (129\,600 \varphi_2 + 48\,600 u_1 - 97,2 + 64\,800 \varphi_2 + 48\,600 u_1 - 97,2) \cdot \left(-\frac{\delta u_1}{4}\right) = 0
\end{aligned}$$

$$(32\,400 \varphi_2 - 91\,800 u_1 + 72,9) \delta u_1 = 0 \quad \forall \delta u_1$$

$$32\,400 \varphi_2 - 91\,800 u_1 + 72,9 = 0 \quad \Big| \quad \times (-1)$$

$$-32\,400 \varphi_2 + 91\,800 u_1 - 72,9 = 0$$

sustav jednadžbi i njegovo rješenje:

$$259\,200 \varphi_2 - 32\,400 u_1 = 38,88$$

$$-32\,400 \varphi_2 + 91\,800 u_1 = 97,2 \quad (\text{sustav je simetričan})$$

$$\varphi_2 = 0,000\,295\,385 \quad \mathcal{E} \quad u_1 = 0,001\,163\,08 \text{ m}$$

vrijednosti momenata savijanja na krajevima štapova:

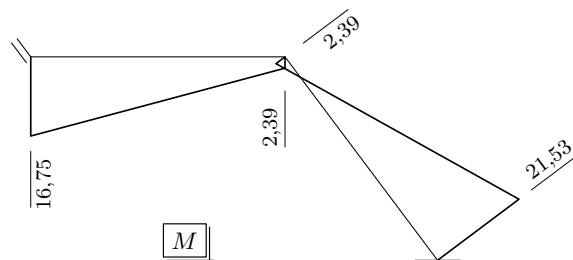
$$M_{1,2} = 64\,800 \cdot 0,000\,295\,385 - 81\,000 \cdot 0,001\,163\,08 + 58,32 = -16,748\,5 \text{ kNm}$$

$$M_{2,1} = 129\,600 \cdot 0,000\,295\,385 - 81\,000 \cdot 0,001\,163\,08 + 58,32 = 2,392\,42 \text{ kNm}$$

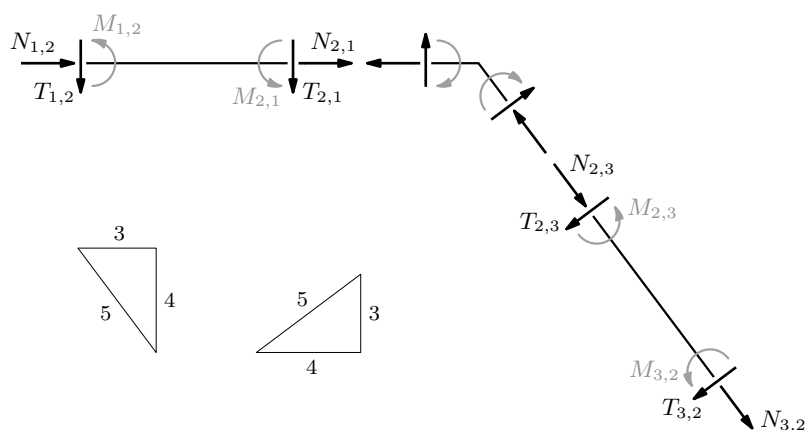
$$M_{2,3} = 129\,600 \cdot 0,000\,295\,385 + 48\,600 \cdot 0,001\,163\,08 - 97,2 = -2,392\,42 \text{ kNm}$$

$$M_{3,2} = 64\,800 \cdot 0,000\,295\,385 + 48\,600 \cdot 0,001\,163\,08 - 97,2 = -21,533\,4 \text{ kNm}$$

dijagram momenata savijanja:



vrijednosti poprečnih sila:



$$T_{1,2} \cdot 5 + M_{1,2} + M_{2,1} = 0 \quad (\text{ravnoteža momenata u odnosu na kraj 2 štapa } \{1,2\})$$

$$T_{1,2} = -\frac{M_{1,2} + M_{2,1}}{5} = -\frac{-16,748\,5 + 2,392\,42}{5} = 2,871\,22 \text{ kN} = -T_{(\xi_{(1,2)}=0^+)}$$

$$T_{1,2} + T_{2,1} = 0 \quad (\text{ravnoteža sila okomitih na os štapa } \{1,2\})$$

$$T_{2,1} = -T_{1,2} = -2,871\,22 \text{ kN} = T_{(\xi_{(1,2)}=5^-)}$$

$$T_{2,3} \cdot 5 + M_{2,3} + M_{3,2} = 0 \quad (\text{ravnoteža momenata u odnosu na kraj 3 štapa } \{2,3\})$$

$$T_{2,3} = -\frac{M_{2,3} + M_{3,2}}{5} = -\frac{-2,392\,42 - 21,533\,4}{5} = 4,785\,16 \text{ kN} = -T_{(\xi_{(2,3)}=0^+)}$$

$$T_{2,3} + T_{3,2} = 0 \quad (\text{ravnoteža sila okomitih na os štapa } \{2,3\})$$

$$T_{3,2} = -T_{2,3} = -4,785\,16 \text{ kN} = T_{(\xi_{(2,3)}=5^-)}$$

vrijednosti uzdužnih sila:

$$-T_{2,1} - \frac{3}{5}T_{2,3} - \frac{4}{5}N_{2,3} = 0 \quad (\text{ravnoteža projekcija sila u čvoru 2 na os } z)$$

$$N_{2,3} = \frac{5}{4} \left(-T_{2,1} - \frac{3}{5}T_{2,3} \right) = -0,000\,147 \simeq 0 = N_{(\xi_{(2,3)}=0^+)}$$

$$N_{2,3} + N_{3,2} = 0 \quad (\text{ravnoteža sila usporednih s osi štapa } \{2,3\})$$

$$N_{3,2} = -N_{2,3} \simeq 0 = N_{(\xi_{(2,3)}=5^-)}$$

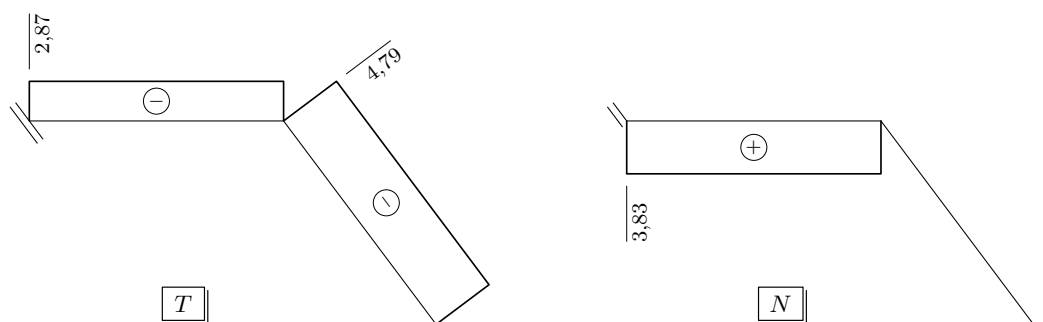
$$-N_{2,1} + \frac{4}{5}T_{2,3} - \frac{3}{5}N_{2,3} = 0 \quad (\text{ravnoteža projekcija sila u čvoru 2 na os } x)$$

$$N_{2,1} = \frac{4}{5}T_{2,3} = 3,828\,131 \text{ kN} = N_{(\xi_{(2,1)}=5^-)}$$

$$N_{1,2} + N_{2,1} = 0 \quad (\text{ravnoteža sila usporednih s osi štapa } \{1,2\})$$

$$N_{1,2} = -N_{2,1} = -3,828\,131 \text{ kN} = -N_{(\xi_{(1,2)}=0^+)}$$

dijagrami poprečnih i uzdužnih sila:



duljina pomaka točke A:

geometrijski postupak:

nepoznanica u_1 (koja to više nije, jer smo je izračunali) duljina je horizontalne komponente pomaka točke A



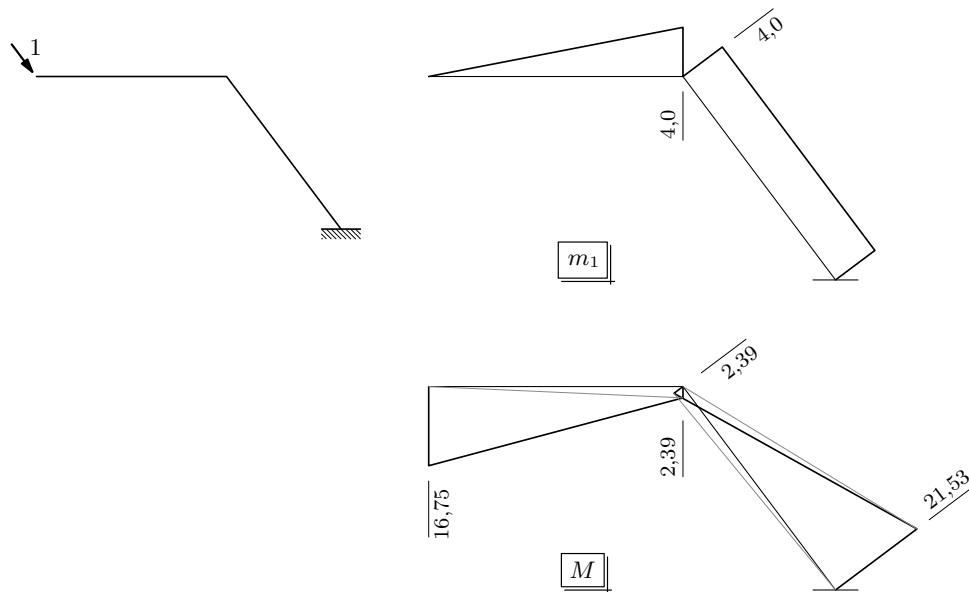
$$\frac{\delta_A}{u_1} = \frac{5}{4}$$

$$\delta_A = \frac{5}{4}u_1 = \frac{5}{4} \cdot 0,001\,163\,08$$

$$= 0,001\,938\,47 \text{ m}$$

$$= 1,94 \text{ mm}$$

metoda jedinične sile \mathcal{E} redukcijski stavak:



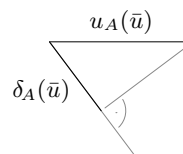
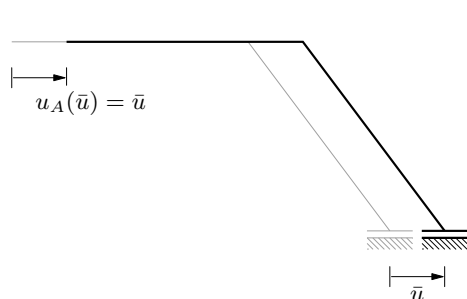
redukcijski stavak: jedinična sila na bilo kojem osnovnom sistemu za metodu sila
 [domaća zabava: objasnite crtanje dijagrama m_1 !]

pomak neke točke zbroj je pomaka od utjecaja momenata savijanja i pomaka od utjecaja prisilnoga pomaka na osnovni sistem za metodu sila (ako prisilni pomak utječe na njega)

utjecaj momenata savijanja:

$$\begin{aligned} \delta_A(M) &= \sum \int \frac{m_1 M}{EI} ds \\ &= \frac{1}{EI} \left[\left(\frac{1}{2} \cdot 16,75 \cdot 5 \right) \left(\frac{1}{3} \cdot 4 \right) (-1) + \left(\frac{1}{2} \cdot 2,39 \cdot 5 \right) \left(\frac{2}{3} \cdot 4 \right) (-1) \right. \\ &\quad \left. + \left(\frac{1}{2} \cdot 2,39 \cdot 5 \right) (4) (-1) + \left(\frac{1}{2} \cdot 21,53 \cdot 5 \right) (4) \right] = 0,000\,738\,477 \end{aligned}$$

utjecaj prisilnoga pomaka na osnovni sistem za metodu sila:

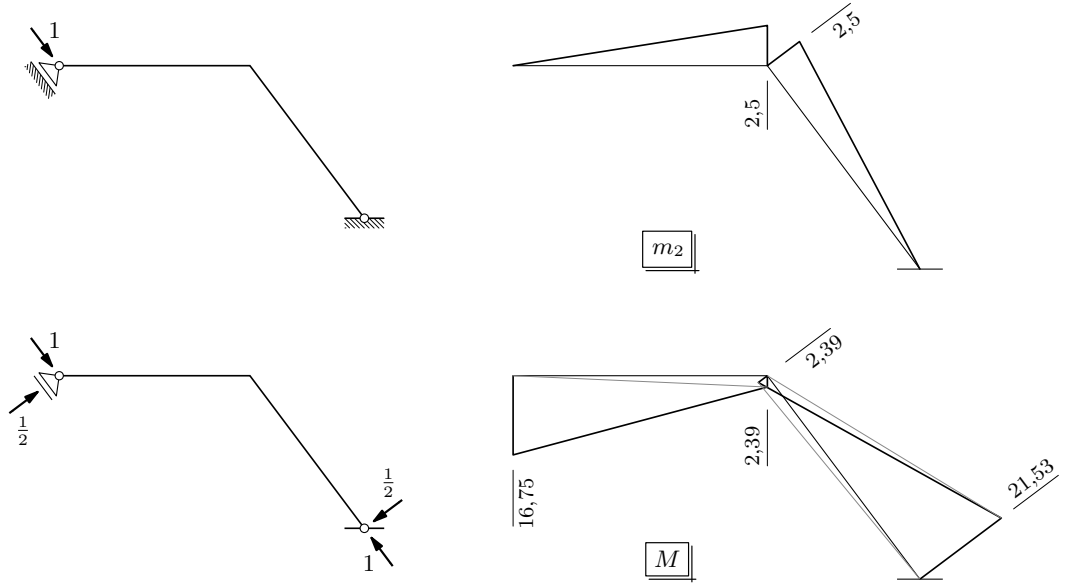


$$\frac{\delta_A(\bar{u})}{u_A(\bar{u})} = \frac{3}{5}$$

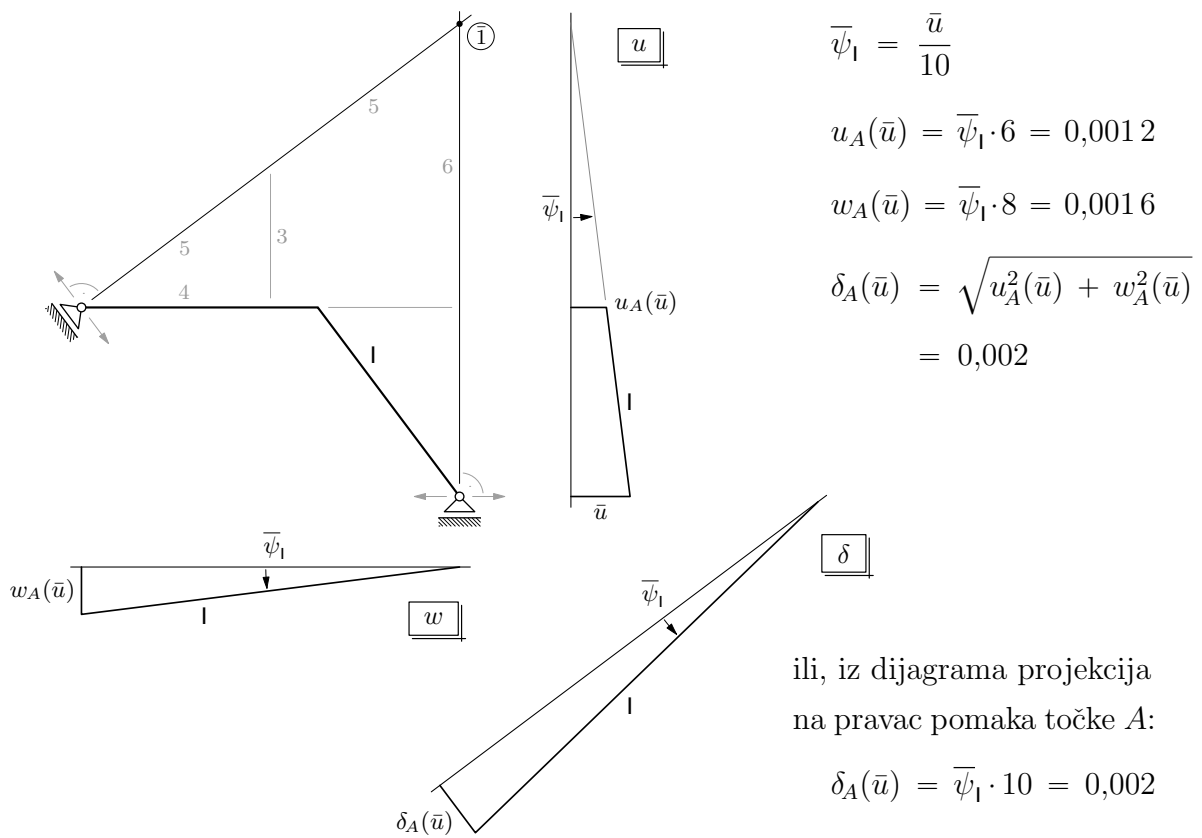
$$\delta_A(\bar{u}) = \frac{3}{5} u_A(\bar{u}) = \frac{3}{5} \bar{u} = 0,001\,2$$

$$\delta_A = \delta_A(M) + \delta_A(\bar{u}) = 0,000\,738\,477 + 0,001\,2 = 0,001\,938\,48 \text{ m} = 1,94 \text{ mm}$$

ili:



$$\begin{aligned} \delta_A(M) &= \frac{1}{EI} \left[\left(\frac{1}{2} \cdot 16,75 \cdot 5 \right) \left(\frac{1}{3} \cdot 2,5 \right) (-1) + \left(\frac{1}{2} \cdot 2,39 \cdot 5 \right) \left(\frac{2}{3} \cdot 2,5 \right) (-1) \right. \\ &\quad \left. + \left(\frac{1}{2} \cdot 2,39 \cdot 5 \right) \left(\frac{2}{3} \cdot 2,5 \right) (-1) + \left(\frac{1}{2} \cdot 21,53 \cdot 5 \right) \left(\frac{1}{3} \cdot 2,5 \right) \right] \\ &= -0,0000614712 \end{aligned}$$

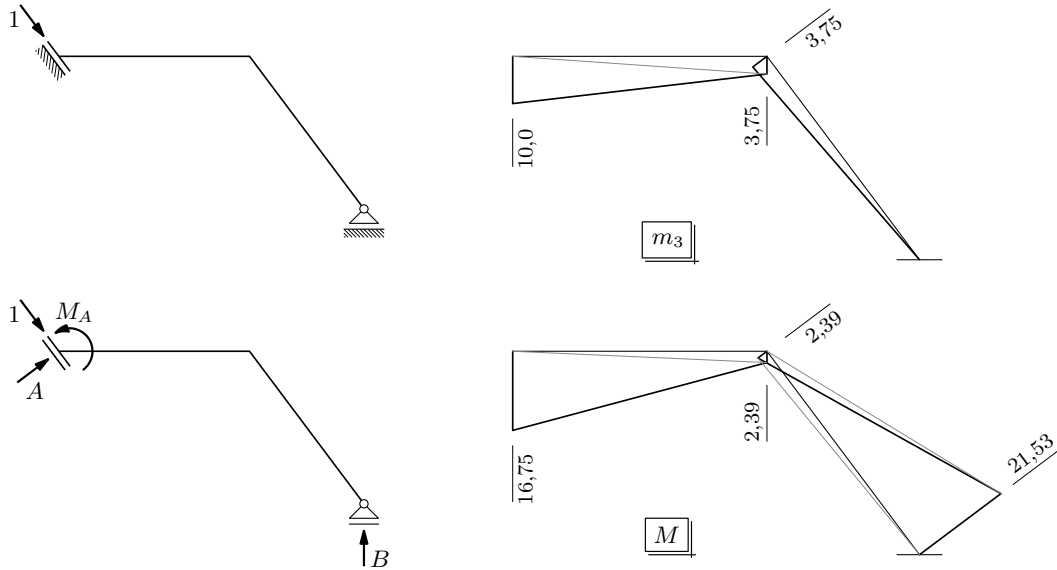


ili, iz dijagrama projekcija na pravac pomaka točke A:

$$\delta_A(\bar{u}) = \bar{\psi}_1 \cdot 10 = 0,002$$

$$\delta_A = \delta_A(M) + \delta_A(\bar{u}) = -0,000\,061\,471\,2 + 0,002 = 0,001\,938\,53 \text{ m} = 1,94 \text{ mm}$$

ili, osnovni sistem za metodu sila na koji prisilni pomak ne utječe:



rješavanje osnovnoga sistema (za metodu sila) na koji djeluje jedinična sila:

$$\begin{aligned} \sum F_x = 0 : \quad & 1^h + A^h = 0 \\ & A^h = -1^h = -\frac{3}{5} \\ & \frac{A}{A^h} = \frac{5}{4} \Rightarrow A = \frac{5}{4} A^h = -\frac{3}{4} = 0,75 \end{aligned}$$

$$\begin{aligned} \sum F_z = 0 : \quad & 1^v - A^v - B = 0 \\ & \frac{A^v}{A^h} = \frac{3}{4} \Rightarrow A^v = \frac{3}{4} A^h = \frac{3}{4} \left(-\frac{3}{5}\right) = -\frac{9}{20} \\ & B = 1^v - A^v = \frac{4}{5} - \left(-\frac{9}{20}\right) = \frac{5}{4} = 1,25 \end{aligned}$$

$$\begin{aligned} \sum M_{/A} = 0 : \quad & M_A + B \cdot 8 = 0 \\ & M_A = -B \cdot 8 = -\frac{5}{4} \cdot 8 = -10 \end{aligned}$$

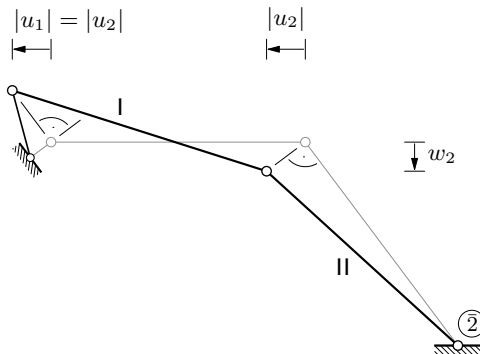
vrijednost momenta savijanja u spoju štapova: $M_{(x=5)} = B \cdot 3 = \frac{15}{4} = 3,75$

$$\begin{aligned} \delta_A = \delta_A(M) &= \frac{1}{EI} \left[\left(\frac{1}{2} \cdot 16,75 \cdot 5 \right) \left(\frac{2}{3} \cdot 10,0 + \frac{1}{3} \cdot 3,75 \right) \right. \\ &\quad + \left(\frac{1}{2} \cdot 2,39 \cdot 5 \right) \left(\frac{1}{3} \cdot 10,0 + \frac{2}{3} \cdot 3,75 \right) \\ &\quad \left. + \left(\frac{1}{2} \cdot 2,39 \cdot 5 \right) \left(\frac{2}{3} \cdot 3,75 \right) + \left(\frac{1}{2} \cdot 21,53 \cdot 5 \right) \left(\frac{1}{3} \cdot 3,75 \right) (-1) \right] \\ &= 0,001\,938\,40 \text{ m} = 1,94 \text{ mm} \end{aligned}$$

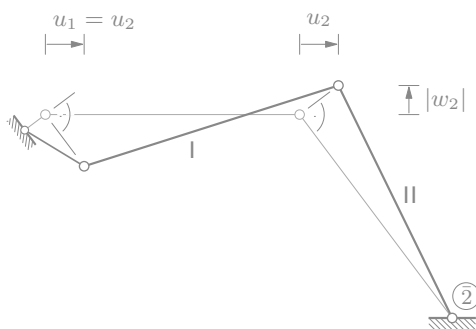
rješavanje pomoću desnoga osnovnog sistema za inženjersku metodu pomakā

(najgornja slika na stranici 2):

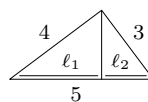
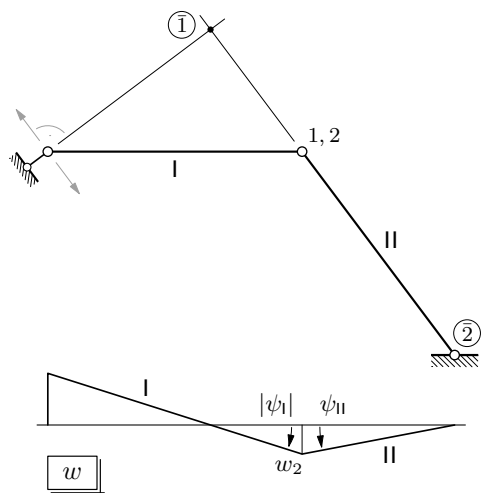
zōra radi, plan pomakā za neovisni translacijski pomak \vec{w}_2 :



uzeli smo, kao što je uobičajeno, da je pomak \vec{w}_2 prema dolje; uzmemo li da je taj pomak prema gore i još da je (za crtež) $w_2 = 3u_2/4 = 3u_1/4$, plan pomakā (kao ni dijagrami projekcija pomakā) neće se razlikovati od plana pomakā (i dijagrama projekcija pomakā) za pomak \vec{u}_1 prikazanoga na stranici 2:



izrazi za kutove $\psi_{i,j}$ kao funkcije neovisnoga translacijskog pomaka w_2 (izvedeni pomoću dijagramā projekcijā pomakā na vertikalnu os):



$$\frac{l_2}{3} = \frac{3}{5}$$

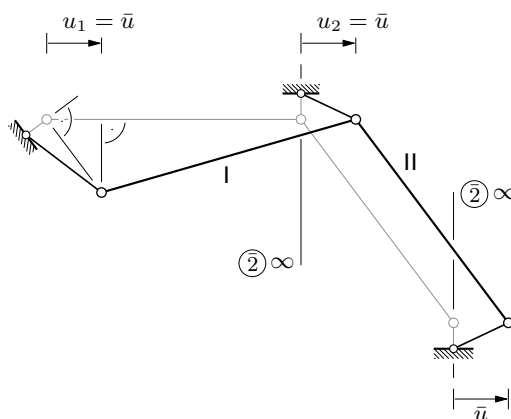
$$l_2 = \frac{9}{5}$$

$$\psi_1 = -\frac{w_2}{l_2} = -\frac{5}{9} w_2 = \psi_{\{1,2\}}$$

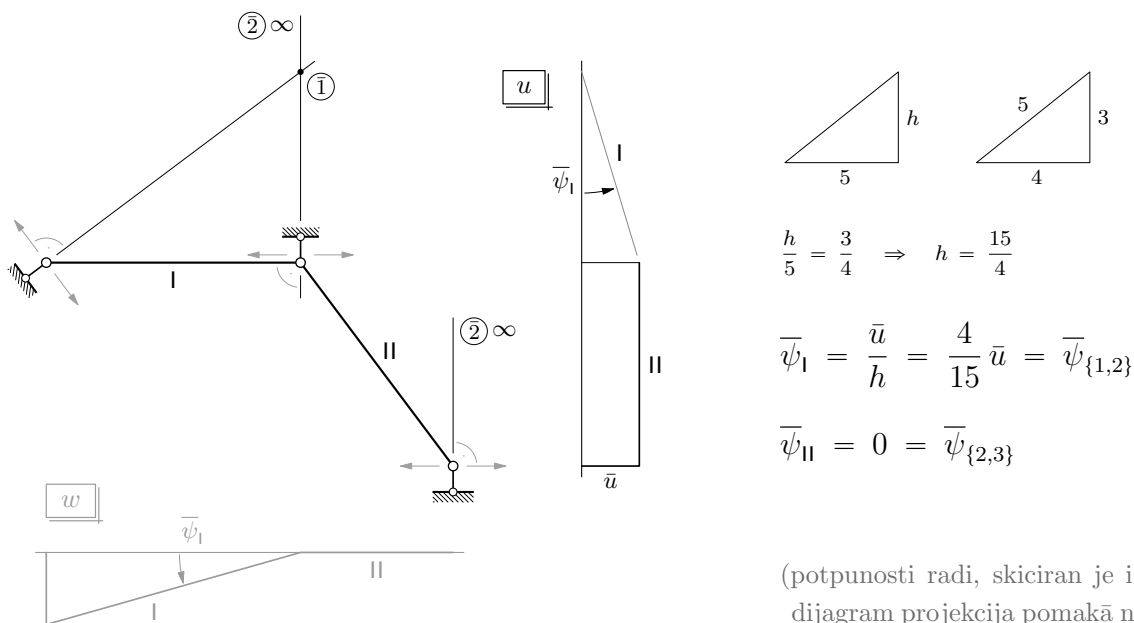
$$\psi_{II} = \frac{w_2}{3} = \psi_{\{2,3\}}$$

(potpunosti radi, skiciran je i dijagram projekcija pomakā na horizontalnu os)

zōra radi, plan pomakā za prisilni pomak ležaja:



izračunavanje kutova $\bar{\psi}_{i,j}$ pomoću dijagramā projekcijā pomakā na horizontalnu os:



vrijednosti momenata upetosti:

$$\begin{aligned} \bar{M}_{1,2} = \bar{M}_{2,1} &= -6 k_{\{1,2\}} \bar{\psi}_{\{1,2\}} = -6 \frac{EI}{5} \frac{4}{15} \bar{u} \\ &= -6 \cdot \frac{162000}{5} \cdot \frac{4}{15} \cdot 0,002 = -103,68 \text{ kNm} \end{aligned}$$

(izrazi za) vrijednosti momenata savijanja na krajevima štapova:

$$\begin{aligned} M_{1,2} &= 2 k_{\{1,2\}} \varphi_2 - 6 k_{\{1,2\}} \psi_{\{1,2\}} + \bar{M}_{1,2} \\ &= 2 \cdot 32400 \varphi_2 - 6 \cdot 32400 \left(-\frac{5}{9} w_2 \right) - 103,68 = 64800 \varphi_2 + 108000 w_2 - 103,68 \end{aligned}$$

$$\begin{aligned}
M_{2,1} &= 4 k_{\{1,2\}} \varphi_2 - 6 k_{\{1,2\}} \psi_{\{1,2\}} + \overline{M}_{2,1} \\
&= 4 \cdot 32\,400 \varphi_2 - 6 \cdot 32\,400 \left(-\frac{5}{9} w_2 \right) - 103,68 = 129\,600 \varphi_2 + 108\,000 w_2 - 103,68
\end{aligned}$$

$$\begin{aligned}
M_{2,3} &= 4 k_{\{2,3\}} \varphi_2 - 6 k_{\{2,3\}} \psi_{\{2,3\}} \\
&= 4 \cdot 32\,400 \varphi_2 - 6 \cdot 32\,400 \cdot \frac{w_2}{3} = 129\,600 \varphi_2 - 64\,800 w_2
\end{aligned}$$

$$\begin{aligned}
M_{3,2} &= 2 k_{\{2,3\}} \varphi_2 - 6 k_{\{2,3\}} \psi_{\{2,3\}} \\
&= 2 \cdot 32\,400 \varphi_2 - 6 \cdot 32\,400 \cdot \frac{w_2}{3} = 64\,800 \varphi_2 - 64\,800 w_2
\end{aligned}$$

jednadžba ravnoteže momenata u čvoru 2:

$$\begin{aligned}
-M_{2,1} + (-M_{2,3}) &= 0 \quad \Big| \quad \times (-1) \\
[129\,600 \varphi_2 + 108\,000 w_2 - 103,68] + [129\,600 \varphi_2 - 64\,800 w_2] &= 0 \\
259\,200 \varphi_2 + 43\,200 w_2 - 103,68 &= 0
\end{aligned}$$

jednadžba rada na virtualnim pomacima:

(„vodeći” je virtualni pomak pomak $\delta \vec{w}_2$ koji odgovara neovisnom translacijskom pomaku \vec{w}_2 , pa je dijagram projekcija (virtualnih) pomaka na vertikalnu os jednak dijagramu prikazanom na najdonjoj slici na stranici 10, uz zamjene $w_2 \rightarrow \delta w_2$ i $\psi_i \rightarrow \delta \psi_i$, a veza je kutova $\delta \psi_{\{i,j\}}$ i orijentirane duljine δw_2 ista kao veza $\psi_{\{i,j\}}$ i w_2 :

$$\delta \psi_{\{1,2\}} = -5 \delta w_2 / 9 \quad \& \quad \delta \psi_{\{2,3\}} = \delta w_2 / 3)$$

$$\begin{aligned}
(M_{1,2} + M_{2,1}) \delta \psi_{\{1,2\}} + (M_{2,3} + M_{3,2}) \delta \psi_{\{2,3\}} &= 0 \\
(64\,800 \varphi_2 + 108\,000 w_2 - 103,68 + 129\,600 \varphi_2 + 108\,000 w_2 - 103,68) \cdot \left(-\frac{5}{9} \delta w_2 \right) \\
+ (129\,600 \varphi_2 - 64\,800 w_2 + 64\,800 \varphi_2 - 64\,800 w_2) \cdot \frac{\delta w_2}{3} &= 0
\end{aligned}$$

$$(-43\,200 \varphi_2 - 162\,667 w_2 + 115,2) \delta w_2 = 0 \quad \forall \delta w_2$$

$$-43\,200 \varphi_2 - 162\,667 w_2 + 115,2 = 0 \quad \Big| \quad \times (-1)$$

$$43\,200 \varphi_2 + 162\,667 w_2 - 115,2 = 0$$

sustav jednadžbi i njegovo rješenje:

$$259\,200 \varphi_2 + 43\,200 w_2 = 103,68$$

$$43\,200 \varphi_2 + 162\,667 w_2 = 115,2 \quad (\text{sustav je simetričan})$$

$$\varphi_2 = 0,000\,295\,026 \quad \& \quad w_2 = 0,000\,629\,844 \text{ m}$$

vrijednosti momenata savijanja na krajevima štapova:

$$M_{1,2} = 64\,800 \cdot 0,000\,295\,026 + 108\,000 \cdot 0,000\,629\,844 - 103,68 = -16,775\,2 \text{ kNm}$$

$$M_{2,1} = 129\,600 \cdot 0,000\,295\,026 + 108\,000 \cdot 0,000\,629\,844 - 103,68 = 2,578\,52 \text{ kNm}$$

$$M_{2,3} = 129\,600 \cdot 0,000\,295\,026 - 64\,800 \cdot 0,000\,629\,844 = -2,578\,52 \text{ kNm}$$

$$M_{3,2} = 64\,800 \cdot 0,000\,295\,026 - 64\,800 \cdot 0,000\,629\,844 = -21,696\,2 \text{ kNm}$$

(Nebitne razlike (iza decimalnoga zareza) između ovih vrijednosti i vrijednosti dobivenih rješavanjem pomoću lijevoga osnovnog sistema posljedice su zanemarivanja pogrešaka zaokruživanja (na šest značajnih znamenaka) u pojedinim koracima proračuna i njihova „gomi-lanja”.)

nastavak je priče (dijagrami \mathcal{E} duljina pomaka) isti kao za lijevi osnovni sistem
(uz lagana prilagođavanja vrijednosti)